The soil carbon in ORCHIDEE

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THE GLOBAL C CYCLE AND ITS SOIL COMPONENT

- The C cycle: a complex cycle composed of different pools.
- These pools interact via different fluxes.







SOILS: MAJOR ACTORS OF THE C CYCLE







SOILS AND GLOBAL CHANGES







SOILS AND GLOBAL CHANGES









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- Split between stomate_litter.f90 and stomate_soilcarbon.f90
 Run at ½ hourly time-step whereas stomate runs at daily time-step.
- Moisture and temperature function calculated in stomate litter.f90

$$\tau = Q_{10}^{(T-Topt)/10}$$

$\theta = Max(0.25, Min(1, M))$ $M = -1.1 * SM^2 + 2.4 * SM - 0.29$





- Input from plants
 through *bm_to_litter* and *turnover*
- Split between above and below ground
- Split into two pools:
 metabolic/structural
- depending on lignin and
- N content of the litter.







 Inputs from litter decomposition in soilcarbon input Distributed into the active and slow pools control by the lignin content.









 Decomposition Structural Litter Litter following 1st order Metabolic kinetics. Litter N_{Min} ∂SON $- = I - k \times SON \times \theta \times \tau$ N_{Min} Active SOM ∂t N_{Min} N_{Min} The flux of N from one N_{Min} Slow SOM N_{Min} pool to another must N_{Min} N_{Min} satisfy the CN target of Passive SOM

the receiving pools





HOW THE NITRIFICATION/DENITRIFICATION PROCESSES ARE REPRESENTED



Peng and Zhu (2006)



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HOW THE NITRIFICATION/DENITRIFICATION PROCESSES ARE REPRESENTED

- Key point -> N outputs fluxes & GHG production
- DNDC is an old model based on Li et al. 1992.
- Design to represent denitrification <u>and</u> decomposition.
- In ORCHIDEE, only the N-related aspects are used but in a simplified way.







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Soil temperature & molsture from submodel of thermal-

hydraulic flow



Li et al., (1992)

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Soil temperature & molsture from submodel of thermal-

hydraulic flow

USED IN ORCHIDEE



Li et al., (1992)

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IMPROVED DNDC

The PnET-N-DNDC Model







IMPROVED DNDC



Li et al., (2000)





IMPROVED DNDC



Li et al., (2000)

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THE ANAEROBIC BALLOON CONCEPT



Li et al., (2000)





THE ANAEROBIC BALLOON CONCEPT

 Table 2. Functions and Parameters for O2 Diffusion and Volumetric Fraction of Anaerobic Microsites (ANVF)

Equation No.	Function	Equation
1	oxygen diffusion coefficient in soil	$D_{s[L]} = D_{air} afps_{[L]}^{3.33} / afps_{max[L]}^{2.0};$
2	oxygen diffusion rate affected by	$\mathbf{D}_{\mathbf{s}[L]} = \mathbf{D}_{\mathbf{s}[L]}$ F_frost; $0 < \mathbf{D}_{\mathbf{s}[L]} < 1$
	frost	if $T > 0$ °C, $F_{frost} = 1.2$;
		if $T \le 0 ^{\circ}C$, $F_{frost} = 0.8$;
		$D_{s[L]} = D_{s[L]} F_{frost}; 0 < D_{s[L]} < 1$
		if $T > 0$ °C, $F_{\text{frost}} = 1.2$;
		if $T \le 0 ^{\circ}C$, $F_{frost} = 0.8$;
3	oxygen partial pressure	$d(pO_{2[L]})/dt = (d(D_{s[L]} d(pO2_{[L]})/dz)/dz - R)/afps;$
4	Volumetric fraction of anaerobic microsites	$anvf_{[L]} = a (1-(b pO_{2[L]}/pO_{2air}));$

a, b, constant coefficients; afps, air-filled porosity; afps_{max}, porosity; anvf, volumetric fraction of anaerobic microsites; D_{air} , oxygen diffusion rate in the air, 0.07236 m²/h [*Beisecker*, 1994]; D_s , oxygen diffusion coefficient in soil; F_frost, frost factor; L, layer number; pO₂, oxygen partial pressure; R, oxygen consumption rate (kg C ha⁻¹h⁻¹); t, time (h); z, soil depth (m).

Li et al., (2000)





THE EQUATIONS

Table 3. Functions and Parameters for Nit	rification
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Equation		
No.	Function	Equation
1	relative growth rate of nitrifiers	$\mu_{g} = \mu_{MAX} ((DOC) / (1 + [DOC]) + F_{m} / (1 + F_{m}));$
2	relative death rate of nitrifiers	$\mu_{\rm d} = a_{\rm MAX} B_{\rm n} / (5 + [\rm DOC]) / (1 + F_{\rm m});$
3	net increase in nitrifiers biomass	$\mu_{\rm b} = (\mu_{\rm g} - \mu_{\rm d}) \mathbf{B}_{\rm n} \mathbf{F}_{\rm t} \mathbf{F}_{\rm m};$
4	nitrification rate	$R_n = R_{max} [NH4] B_n pH;$
5	temperature factor	$F_t = ((60-T)/(25.78)^{3.503} e^{(3.503 (T-34.22)/(25.78))};$
6	moisture factor	if wfps > 0.05 $F_m = 1.01 - 0.21$ wfps;
		if wfps ≤ 0.05 $F_m = 0;$
7	NO production from	$NO = .0025 R_n F_t;$
8	N ₂ O production from nitrification	$N_2O = 0.0006 R_n F_t$ wfps;

 a_{MAX} , maximum death rate for nitrifiers (1.44 1/d [from *Blagodatsky and Richter*, 1998]); B_n , biomass of nitrifiers (kg C/ha); [DOC], concentration of dissolved organic C (kg C/ha); F_m , moisture factor; F_v , temperature factor; [NH4], concentration of ammonium (kg N/ha); NO, NO production from nitrification; N₂O, N₂O production from nitrification [*Ingwersen et al.*, 1999]; pH, soil pH; R_n , nitrification rate; R_{max} , maximum nitrification rate (1/h); T, soil temperature (°C); wfps, water-filled porosity; μ_{MAX} , maximum growth rate for nitrifiers (4.87 1/d [from *Blagodatsky and Richter*, 1998]); μ_b , net increase in nitrifiers biomass; μ_d , relative death rate of nitrifiers; μ_g , relative growth rate of nitrifiers.





THE EQUATIONS

Equation Function Equation No. $\mu_{NOx} = \mu_{NOx(max)} [DOC]/(Kc+[DOC]) [No_x]/(Kn+[NO_x]);$ relative growth rate of Nox 1 denitrifiers $\mu_{g} = F_{t} (\mu_{NO3} F_{PH1} + \mu_{NO2} F_{PH2} + \mu_{NO} F_{PH2} + \mu_{N20} F_{PH3};$ $F_{t} = 2^{((T-22.5)/10)};$ relative growth rate of total 2 denitrifiers $F_{PH1} = 1 - 1 / (1 + e^{[pH-4.25/0.5]});$ $F_{PH2} = 1 - 1 / (1 + e^{[pH-5.25/1.0]});$ $F_{PH3} = 1 - 1 / (1 + e^{[pH-6.25/1.5]});$ 3 $R_g = \mu_g B_d;$ denitrifier growth rate, death rate, and consumption rate of soluble $\mathbf{R}_{d} = \mathbf{M}_{c} \mathbf{Y}_{c} \mathbf{B}_{d};$ carbon $R_{c} = (\mu_{a} / Y_{c} + M_{c}) B_{d};$ consumption rates of N oxides $\mathbf{R}_{NOx} = (\mu_{NOx}/Y_{NOx} + \mathbf{M}_{NOx} [No_x]/[N]) \mathbf{B}_d;$ 4 5 $q_N = R_\alpha / CN;$ nitrogen assimiliation rate $v = D_{max}$ afps (1 - anvf) $F_{elav} 2^{T/20}$; 6 gas diffusion factor $F_{elav} = 0.13 - 0.079$ clay;

Table 4. Functions and Parameters for Denitrification

afps, air-filled porosity; anyf, volumetric fraction of anaerobic microsites; B_a, denitrifier biomass (kg C/m³); clay, clay fraction in the soil; CN, C/N ratio in denitrifiers (3.45 [Van Verseveld and Stouthamer 1978]); De, consumption rate of soluble carbon by denitrifiers (kg C m⁻³h⁻¹); D_{max}, maximum diffusion rate in air (m^2/h) ; D_{NOS} , consumption rate of N oxides by denitrifiers (kg C m³h⁻¹); [DOC], so!uble C concentration (kg C/m³); F_{elav}, clay factor; F_v, temperature factor; F_{PH1}, pH factors for NO₃ denitrifiers; F_{PH2}, pH factors for NO₂ and NO denitrifiers; F_{pit}, pH factors for N₂O denitrifiers; Kc, half-saturation value of soluble carbon (0.017 kg C/m³ [Shan and Coulman, 1978]); Kn, half-saturation value of N oxides (0.083 kg N/m³ [Shan and Coulman, 1978]); M., maintenance coefficient on carbon (0.0076 kg N kg⁻¹h⁻¹ [Van Verseveld et al., 1977]); [N], concentration of all NO_x (kg N/m³); [No_x], concentration of for NO₃, NO₂, NO and N₂O (kg N/m³); pH, soil pH; q_n , nitrogen assimilation rate (kg N ha⁻¹h⁻¹); T, soil temperature (°C); v, gas diffusion factor (%); Y_a , maximum growth rate of denitrifiers on soluble carbon (0.503 kg C/kg C [Van Verseveld et al., 1977]); M_{Nox}, maintainance coefficient on N oxides (0.09, 0.035 and 0.079 kg N/kg/ for NO₃⁻, NO₂⁻ (+NO*) and N₂O, respectively, based on Van Verseveld et al. [1977]); R_d , denitrifier death rate; R_e , denitrifier growth rate; Y_{NOx} , maximum growth rate on N oxides (0.401, 0.428 and 0.151 kg C/kg N for NO₃⁻, NO₂⁻ (+NO*) and N₂O, respectively, based on Van Verseveld et al. [1977]); μ_a , relative growth rate of total denitrifiers (1/h); μ_{NO3} , μ_{NO2} . μ_{N0}, μ_{N20} , relative growth rate of NO₃⁻, NO₂⁻, NO-, and N₂O denitrifiers; μ NOx, relative growth rate of NO_x denitrifiers (1/h); $\mu_{NOs(max)}$, maximum growth rates (0.67 1/h for NO₃, NO₂ denitrifiers, and 0.34 1/h for NO and N₂O denitrifiers, based on *Hartel and Alexander* [1987]). The parameters are shared by NO₂ and NO due to the lack of data for NO.





WHAT IS DONE IN ORCHIDEE

- Implemented by Zaehle et al., (2010)
- At that time, no DOC and no soil C discretization.
- Active C pools used instead of DOC.
- Gas diffusion is calculated using a fixed soil depth value of 20cm.
- Several parameters tuned.
- With Nicolas, we decided to let the original parameter values.





HOW GOOD ARE EARTH SYSTEM MODELS TO REPRESENT SOIL C STOCK



HOW GOOD ARE EARTH SYSTEM MODELS TO REPRESENT SOIL C STOCK





MEAN RESIDENCE TIME

Based on 14C data, ESM MRT are overestimated by ~40%

Table 1. Global soil carbon stocks and carbon uptake for CMIP5 models that experienced a quadrupling of atmospheric CO₂ from a preindustrial value of 285 ppm over a period of 140 years.

			%						¹⁴ C-imposed correction factors [†]			
ESM	Initial SOC (Pg C)	% change in SOC	change in SOC after ¹⁴ C con- straint	¹⁴ C- imposed sink reduction (%)	τ _{slow} (year)*	^τ passive (year)	r _f	r _s	$\tau_{\rm slow}$	⁷ passive	r _f	r _s
CESM1	571	63	51	19	56 ±	1310 ±	0.06 ±	0.33 ±	_	3.7 ±	_	0.34 ±
(BGC)	571	0.5	5.1	15	16	241	0.05	0.05		1.5		0.75
GFDL-	10.4.4	00	2.2	07	231 ±	1 ± 0.17 6 0.07	0.17 ±	7 ± _ 7	16 ±	-	0.06 ±	
ESM2M	1344	26	3.3	8/	196		0.07		18		0.14	-
HadGE	1000	<u> </u>		10	208 ±		0.12 ±		17 ±		0.07 ±	
M2-ES	1028	63	33	46	84	-	0.07	-	12	-	0.32	-
IPSL-					210 +	1101 +	0.06 +	0.20 +		14 +		0.07 +
CM5A-	1340	27	25	5.9	210 -	247	0.00 ±	0.29 ±	-	14 -	-	0.07 ±
LR					82	347	0.03	0.07		8.3		0.14
MRI-	1400	20		40	347 ±	1065 ±	0.17 ±	0.10 ±		13 ±	0.46 ±	0.34 ±
ESM1 [‡] 1403	36 2	22	40	117	257	0.09	0.06	-	7.2	0.79	0.74	
Mean [§]	1137 ±	32 ±	18 ±	40 ±	212 ±	1185 ±	0.12 ±	0.24 ±	16.5 ±	10.2 ±		
	312	18	12	27	104	123	0.06	0.12	0.5	4.6	-	-

* τ_{slow} , τ_{passive} denote the turnover time, and r_{f} , r_{s} denote the transfer coefficient from the fast to the slow pool and from the slow to the passive pool, respectively. Reported values were estimated as an area-weighted mean and standard deviation of all model grid cells. The mean and standard deviation of the ¹⁴C-imposed correction factors were derived from using the ¹⁴C observations at each site in a single optimization and then averaging these scalar adjustments across the set of 157 optimizations. The ¹⁴C-constrained sink reduction and correction factor for MRI were based on an inverse analysis that changed the pool size of both slow and passive pools. The reported percentage change in SOC and sink reduction were derived from transient simulations starting at steady state with the reduced complexity model. See methods in the supporting materials. SThe multimodel mean and standard deviation were estimated using the mean value from each of the five ESMs.



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He et al., 2016



A NEW SOIL SCHEME FROM THE MICT BRANCH

- For CMIP6, some LSMs will have permafrost C, explicit N cycle and perhaps both
- All the necessary piece of code exist within the « orchidee environment »
- Opportunity to benefit from the huge effort done in the MICT branch by many colleagues (Dan Zhu, Philippe Ciais, Matthieu Guimberteau, Charlie Koven, …)

Only an option in the trunk controlled by OK_SOIL_CARBON_DISCRETIZATION





WHAT DO WE TOOK FROM MICT?

- Several options are available in MICT but not in the trunk (fire, grassland management, permafrost C)
- Focus on permafrost C
- Not only adding « frozen C »
- Soil C is discretized
- Diffusion is added (including bioturbation and cryoturbation)
- Temperature effect on SOC mineralization
- When frozen, nroot is set to -> impact on water stress and on transpiration.
- Optional
 - Zimov effect
 - Insolation effect (thermal conductivity affected by SOC)





- Soil organic N is also discretized
- Mineral N is not
- No effect on N plant uptake





- Representation of the soil C/N profile
- Lateral outputs of C (DOC, Erosion)
- Representation of Priming effect.
- Carbon isotopes (¹⁴C and ¹³C)
- Peatlands





- Any models used for CMIP5 represent the soil C profiles.
- A substantial part of the soil C stored in deep layers (Jobbagy and Jackson, 2000)
- Deep C dynamic different from surface C (Fontaine et al., 2007)
- In ORCHIDEE any C is lost by drainage or runoff instead of the importance of allochtonous C in the aquatic ecosystems functionning (Cole et al., 2007, Bianchi et al., 2011)





Soil Carbon discretization

ORCHIDEE SVN r3340







Soil Carbon discretization

Soil C discretized using the same layers than hydrology scheme (11 layers). A new pool introduced (DOC)



Soil Carbon discretization

Adsorption of DOC following initial mass isotherms

$$DOC_{ads} = Kd \times DOC_{free}$$

- DOC transported within the profile following the water movements (Futter et al., 2007) and exported following the runoff and the drainage fluxes
- POC and DOC transported using the second Fick's law

$$F_D = -D \times \frac{\partial^2 C}{\partial z^2}$$



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SITE SIMULATIONS



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SITE SIMULATIONS



Camino-Serrano et al., (2018)







Guenet et al., (In prep)

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THANK YOU FOR YOUR ATTENTION!



