

# Modification of the aerodynamic resistance formulation

*A possible solution for reducing the bias on evaporation*

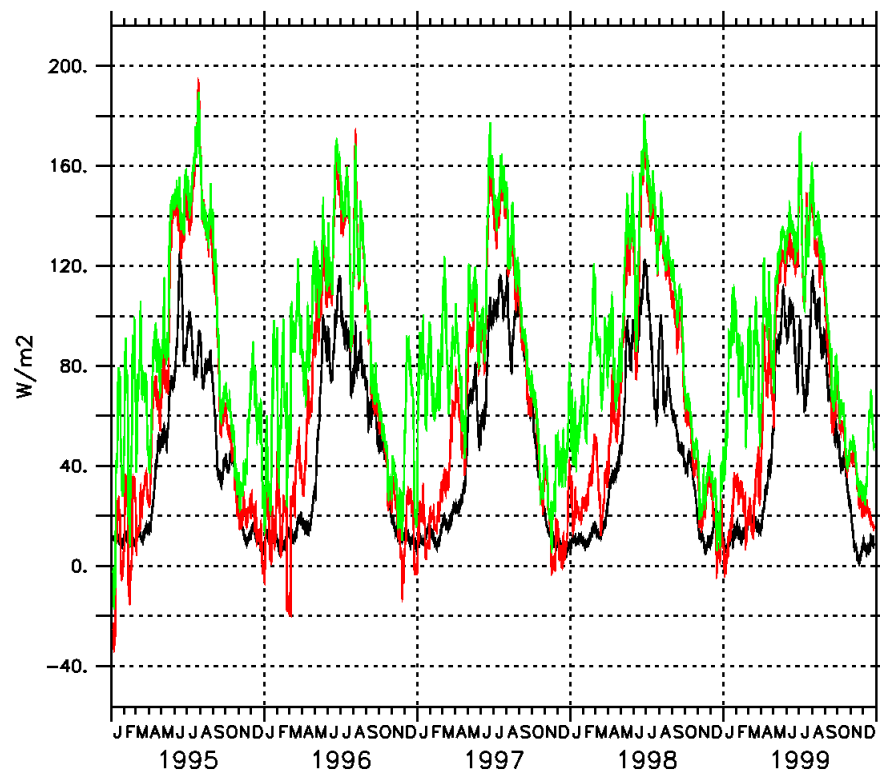
N. Vuichard - LSCE



# Context

- Shifting from the 2-layer hydrological scheme to the 11-layer one increases latent heat flux for some PFT's

- That is due to the evaporative component
- It acts at winter time for deciduous trees when no canopy coverage



— OBS  
— 2-layer  
— 11-layer

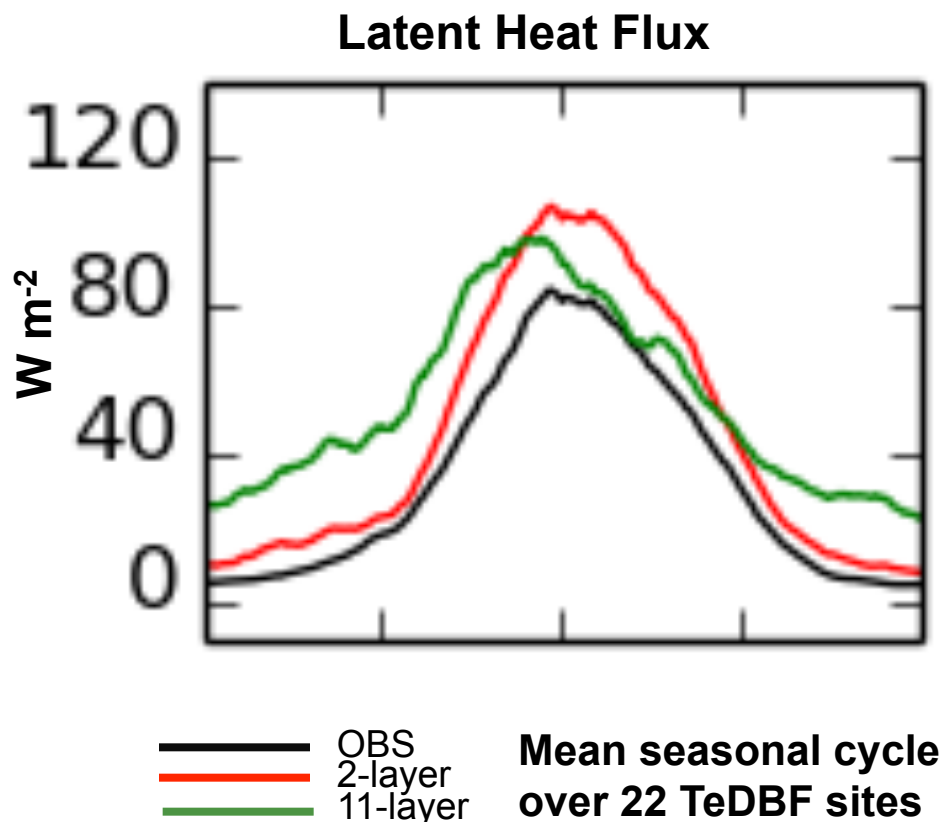
**Latent Heat flux @ Walker Branch site (TeDBF)**



# Context

- Shifting from the 2-layer hydrological scheme to the 11-layer one increases latent heat flux for some PFT's

- That is due to the evaporative component
- It acts at winter time for deciduous trees when no canopy cover



## How evaporation is represented ?

- In the 2-layer scheme, there is an explicit soil resistance to evaporation
- In the 11-layer scheme, the potential evapotranspiration is the flux set as a boundary condition to the diffusion scheme.
  - Either the potential evapotranspiration can be supplied
  - Either a minimal evaporation flux is defined by setting the soil water content of the first layer to the residual

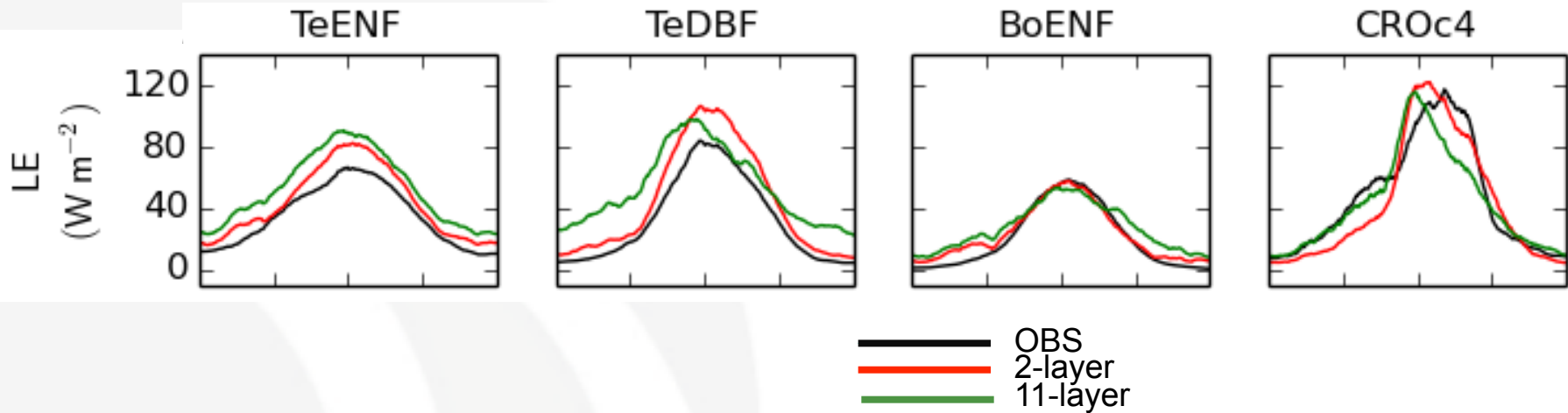
⇒ ***Different schemes, no direct comparison***



## Many sources of uncertainties

- Only measurements of the evapotranspiration, no direct measurements of evaporation
- Evaporation and transpiration components are driven by the LAI which is computed by ORCHIDEE  
⇒ Differences between observed and modelled LAI
- Observed Energy budget is not closed by approx. 15-20%

# Latent heat flux on different vegetation types



- Good performance of the 11-layer scheme over cropland sites, even during bare soil periods (only evaporation, no transpiration)



# Searching for possible processes ...

- That may explain the bias on evaporation
- Modelled differently for crops and forests PFT within ORCHIDEE

⇒ ***Aerodynamic resistance and the parameterization of the roughness height***

$$r_a = \frac{1}{\kappa^2 u_a} \left[ \ln \left( \frac{z - d_0}{z_{0m}} \right) \ln \left( \frac{z - d_0}{z_{0v}} \right) \right]$$

**where**

- z is measurement height (m)
- $u_a$  is wind speed ( $\text{ms}^{-1}$ )
- k von Karman's constant
- $d_0$  is displacement height
- $z_{0m}$  and  $z_{0v}$  the roughness heights for momentum and water vapor transfer



# Roughness height calculation in ORCHIDEE

- Calculation of the averaged  $z_0$  for a grid point
  - For true bare soil and “bare soil” of vegetated PFTs  
 $z_0 = 0.01 \text{ m}$  *weighted by tot\_baresoil*
  - For grass and crops  
 $z_0 = 1/16 * \text{height}$  *weighted by veget*
  - For trees  
 $z_0 = 1/16 * \text{height}$  *weighted by veget\_max*
- ⇒ *One assumes that the trunk and the branches impact as a full canopy coverage on  $z_0$*
- Search for literature supporting that  $z_0$  varies with LAI
  - Ershadi et al. (2015) uses the formulation of Su et al. (2001)
  - An evaluation of different  $z_0$  formulations by Liu et al. (2007)



# Formulation of Su et al . (2001)

- Roughness height for momentum transfer

$$z_{0m} = h_c \left( 1 - \frac{d_0}{h_c} \right) \exp \left( -\frac{\kappa}{\eta} \right)$$

where

–  $h_c$  is the canopy height

–  $\eta$  is the ratio of friction velocity to wind speed, defined as function of LAI

- Roughness height for water vapor transfer

$$z_{0h} = z_{0m} / \exp(\kappa B^{-1})$$

$$\kappa B^{-1} = \frac{\kappa C_d}{4C_t \beta (1 - \exp(-\frac{n_{ec}}{2}))} f_c^2 + 2f_c f_s \frac{\kappa \eta z_{0m} / h_c}{C_t^*} + \kappa B_s^{-1} f_s^2$$

where

$f_c$  the fraction of canopy coverage and  $f_s$  the fraction of soil coverage

# Impacts on the energy budget

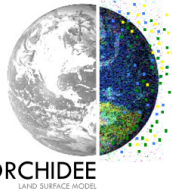
- On the latent heat flux

$$L.E_s^t = L\rho |\vec{v}| C_d \beta (q_1^t - q_{sat}(T_s^t))$$

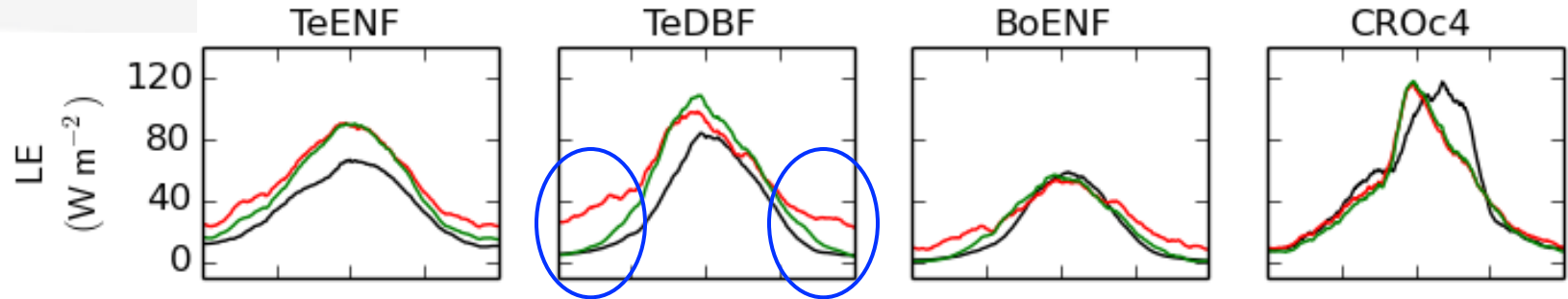
- On the sensible heat flux

$$F_{H,s}^t = \rho |\vec{v}| C_d (H_1^t - H_s^t)$$

With  $C_d$  the drag coefficient =  $(r_a u_a)^{-1}$



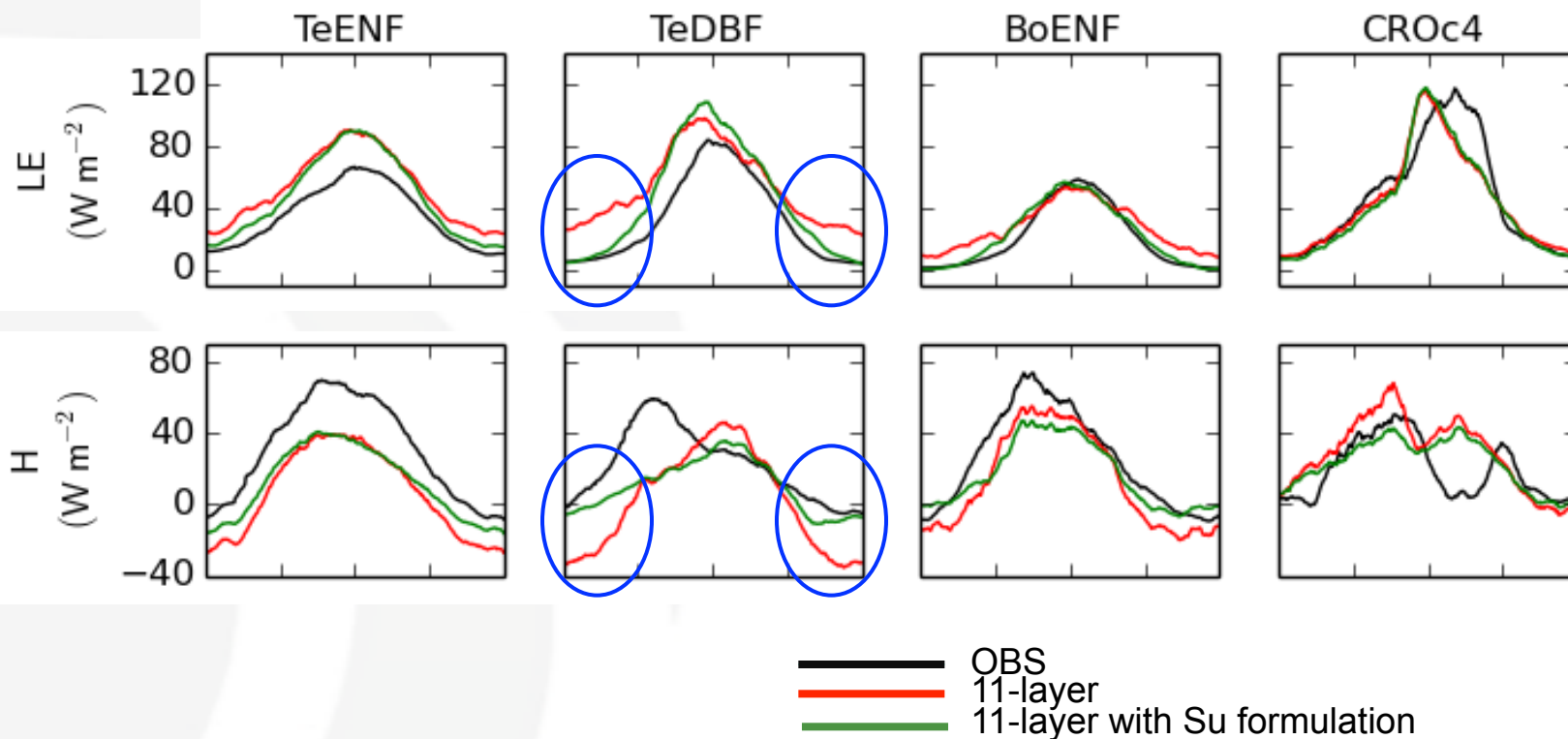
# Evaluation at site level (1)



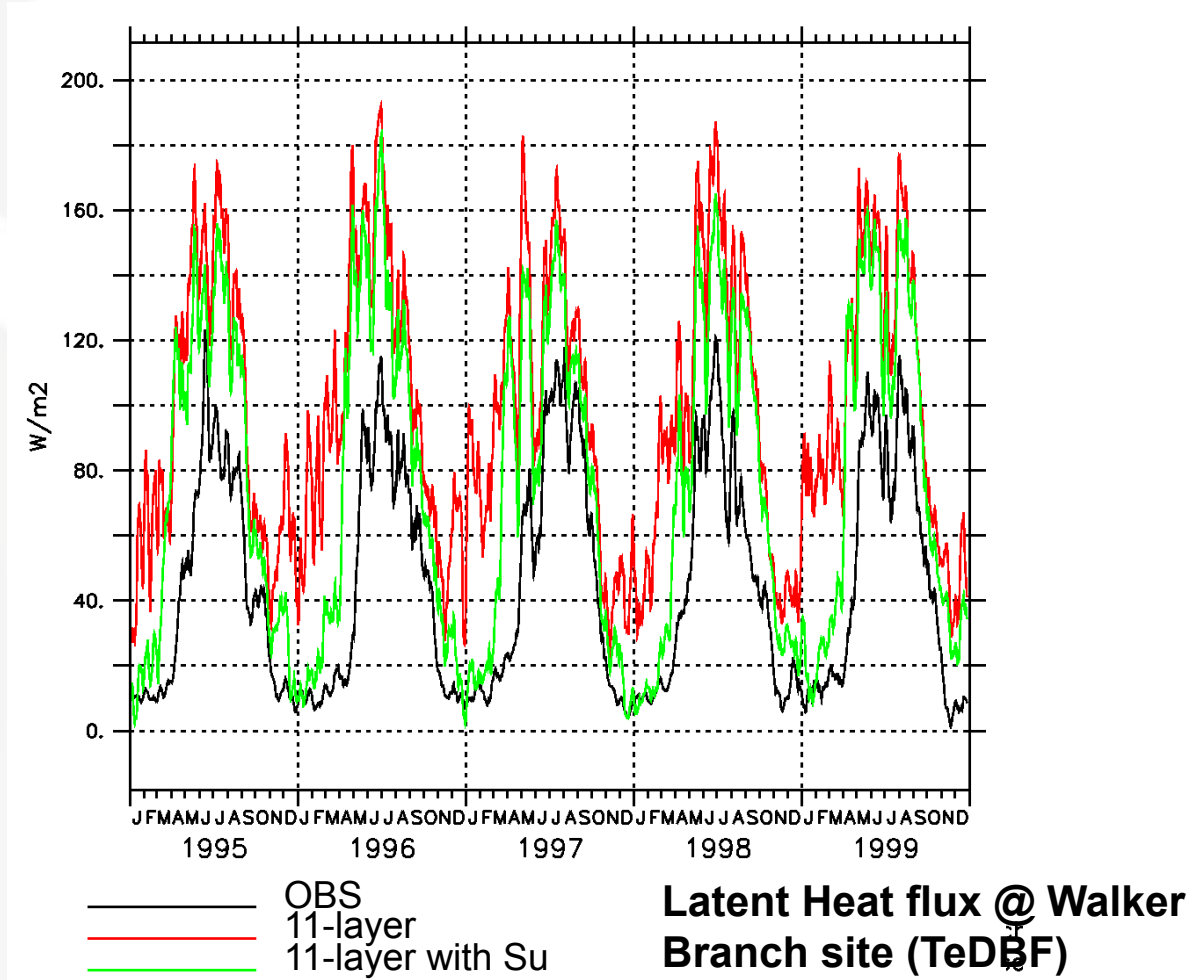
— OBS  
— 11-layer  
— 11-layer with Su formulation



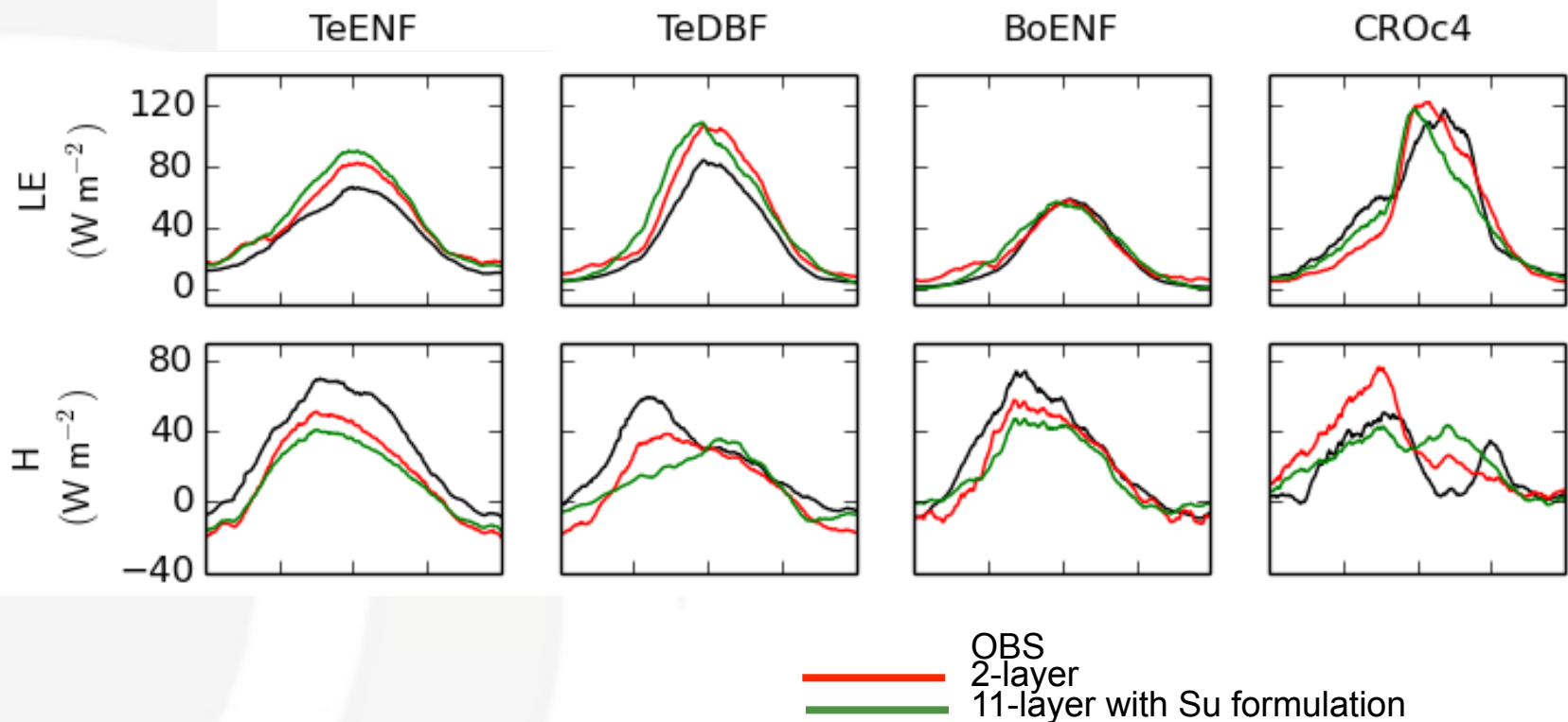
# Evaluation at site level (1)



# Evaluation at site level (1)



# Evaluation at site level (2)



# Conclusion & Perspectives

- Accounting for a roughness height varying with the canopy coverage
  - can correct alone for the bias on evaporation
  - a soil resistance can be added but it is not needed
- Implementation of the formulation of Su et al.
  - Relatively complex
  - More simple formulations could be envisaged ?
- Work on the water stress on GPP
  - Can now be envisaged

# Conclusion & Perspectives

- Accounting for a roughness height varying with the canopy coverage
  - can correct alone for the bias on evaporation
  - a soil resistance can be added but it is not needed
- Implementation of the formulation of Su et al.
  - Relatively complex
  - More simple formulations could be envisaged ?
- Work on the water stress on GPP
  - Can now be envisaged

**Thank you !**

***Thanks to Vladislav Bastrikov for the post-treatment scripts and plots***