

# Infiltration sols gelés

C. Ottlé et al., ...

Infiltration calculée en fonction de la quantité d'eau liquide dans le sol en niveau de la surface , via conductivité hydraulique au niveau de la surface

Problème: qd  $mcl = 0$  à l'interface sol-atmosphère, infiltration = 0

Différents tests pour permettre une infiltration dans ces situations :

### 1. Représentation d'une variabilité sous maille en limitant la fraction de gel à un certain pourcentage de la maille :

Application au calcul de la fraction d'eau gelée par couche et par tile de sol :  
profil\_froz\_hydro\_ns dans la routine hydrol\_soil\_froz.f90

$\text{profil\_froz\_hydro\_ns}(ji,jsl,ins) = \text{MIN}(\text{maxfroz\_hydro}, 1. - \text{r\_std} - x)$

x étant la fraction d'eau non gelée, et nous avons testé des valeurs de 0.8, 0.9 et 1 pour la variable seuil maxfroz\_hydro.

Peu d'impact pour des valeurs > 80%

### 2. Faire varier ce seuil avec la profondeur :

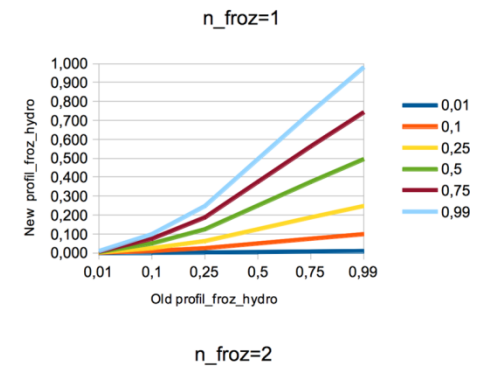
Premier test avec un profil exponentiel du seuil , pas concluant car affecte identiquement toutes les régions quel que soit l'intensité du gel

### 3. Faire varier la correction en fonction de l'intensité du gel (quand toute la colonne de sol (2m) est gelée , pas de correction..)

## Calcul d'un indice d'intensité du gel, intégré sur les 2 m de sol :

```

DO jsl=1,nslm
froz_frac_moy(:) = froz_frac_moy(:) + dh(jsl)*profil_froz_hydro_ns(:,jsl,ins)
denom(:) = denom(:) + dh(jsl)
ENDDO
froz_frac_moy(:) = froz_frac_moy(:)/denom(:)
    
```



## Correction de la fraction d'eau gelée dans chacune des couches à l'aide cet indice :

```

DO jsl=1,nslm
profil_froz_hydro_ns(:,jsl,ins) = profil_froz_hydro_ns(:,jsl,ins) * froz_frac_moy(:)**(1/n_froz)
ENDDO
    
```

Meilleurs résultats mais obtenus avec une valeur de nfroz=0.5, impacts significatifs sur les débits du Danube et du Mississipi

## 4. Prise en compte de l'humidité du sol (Gray et al., 2001),

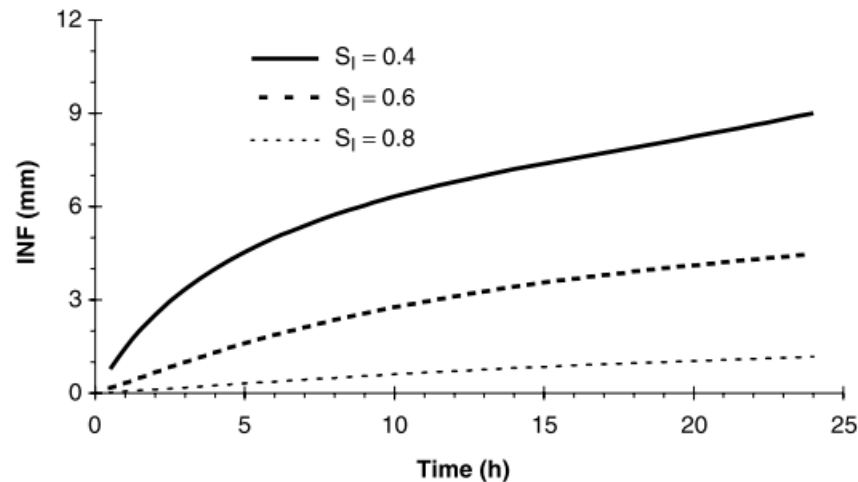


Figure 7. Variation in cumulative infiltration, INF, with time into a frozen, silty clay soil with  $S_1 = 0.4, 0.6, 0.8$  and  $T_1 = -6^\circ\text{C}$ ,  $S_0 = 0.75$ . Infiltration at hour 12 is 6.8 mm, 3.1 mm and 0.7 mm for  $S_1 = 0.4, 0.6, 0.8$  respectively

Calcul d'un indice d'humidité moyen, intégré sur le 1<sup>er</sup> mètre de sol :

```
DO jsl=1,nslm
  DO ji=1,kjpindex
    mc_ns(ji,jsl,ins)=mc(ji,jsl,ins) / mcs(njsc(ji))
  ENDDO
ENDDO

smtot_moy(:)=zero
denom=zero
DO jsl=1,nslm-1
  smtot_moy(:)=smtot_moy(:)+dh(jsl)*mc_ns(:,jsl)
  denom=denom+dh(jsl)
ENDDO
smtot_moy(:)=smtot_moy(:)/denom
```

Correction de la fraction d'eau gelée dans chacune des couches en rajoutant cet indice :

```
DO jsl=1,nslm
  profil_froz_hydro_ns(:,jsl,ins)=profil_froz_hydro_ns(:,jsl,ins) * froz_frac_moy(:)**froz_frac_corr * smtot_moy(:)**smtot_corr
ENDDO
```

Différents tests faits par Vlad :

"frz" - OK\_FREEZE=y, READ\_REFTEMP=y

"frz.frzcor2" - OK\_FREEZE=y, READ\_REFTEMP=y, froz\_frac\_corr=2

"frz.frzcor2.maxfrz09" - OK\_FREEZE=y, READ\_REFTEMP=y, froz\_frac\_corr=2, max\_froz\_hydro=0.9

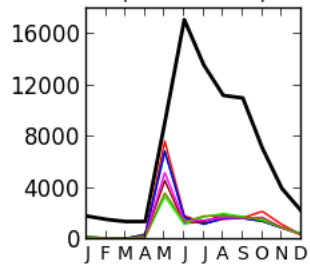
"frz.smtotcor1" - OK\_FREEZE=y, READ\_REFTEMP=y, smtot\_corr=1

"frz.frzcor2.smtotcor1" - OK\_FREEZE=y, READ\_REFTEMP=y, froz\_frac\_corr=2, smtot\_corr=1

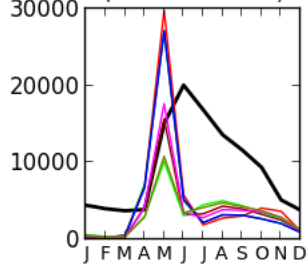
"frz.smtotcor2" - OK\_FREEZE=y, READ\_REFTEMP=y, smtot\_corr=2

"frz.frzcor1.smtotcor2" - OK\_FREEZE=y, READ\_REFTEMP=y, froz\_frac\_corr=1, smtot\_corr=2

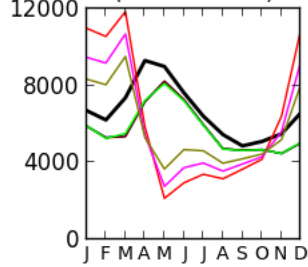
1: Yukon (1991-1995)  
(Pilot station)



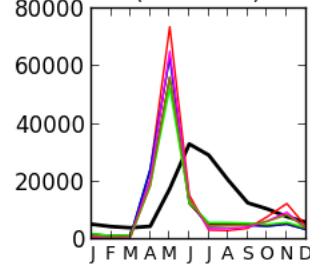
5: McKenzie (1991-2010)  
(Arctic red river)



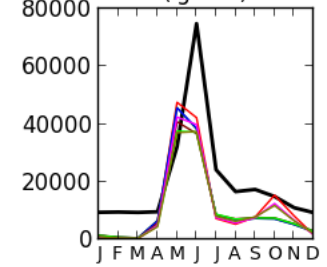
7: Danube (1991-2010)  
(Ceatal Izmail)



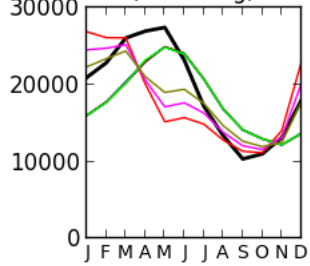
9: Ob (1991-2010)  
(Salekhard)



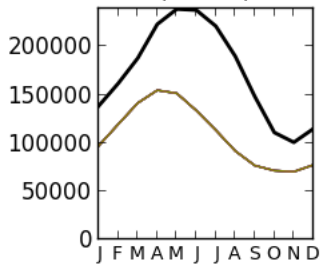
11: Yenisei (1991-2010)  
(Igarka)



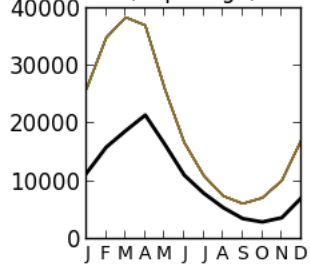
2: Mississippi (1991-2010)  
(Vicksburg)



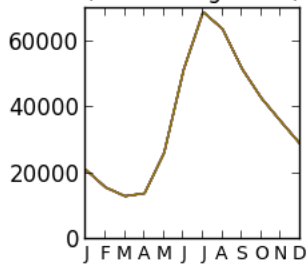
3: Amazon (1991-2005)  
(Obidos)



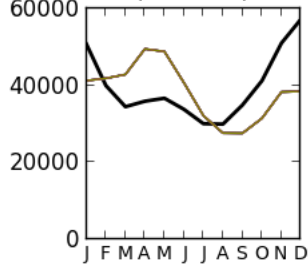
4: Tocantins (1991-2010)  
(Itupiranga)



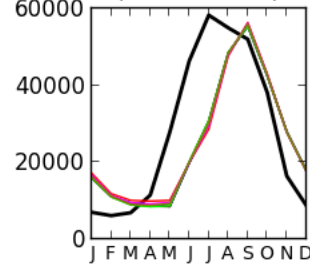
6: Orinico (1991-1989)  
(Puente Angostura)



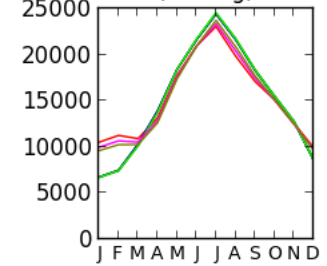
8: Congo (1991-2010)  
(Kinshasa)



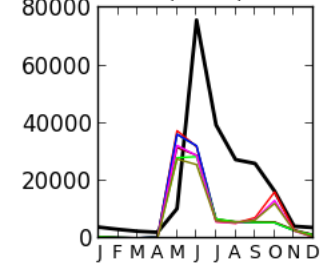
10: Brahmaputra (1991-1991)  
(Bahadurabad)



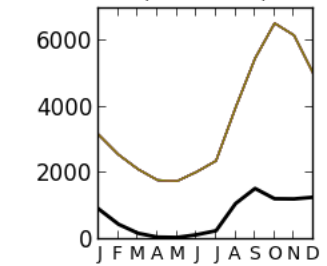
14: Yangzi Jiang (1991-1988)  
(Datong)



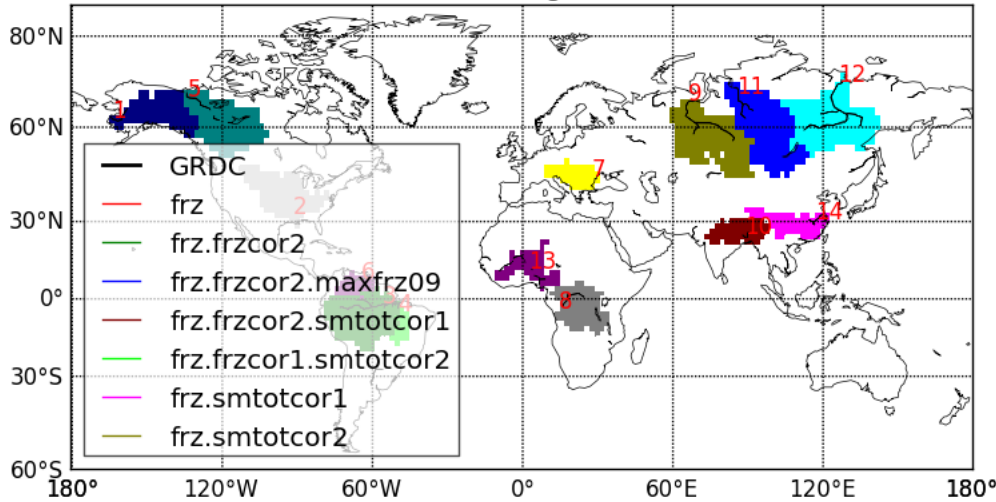
12: Lena (1991-2010)  
(Kusur)

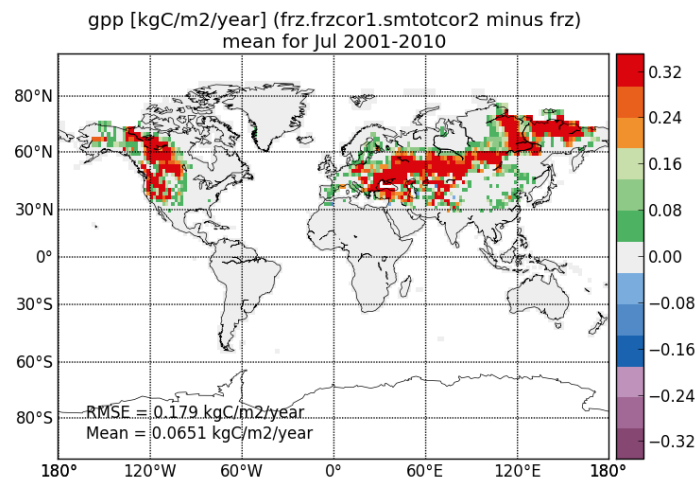
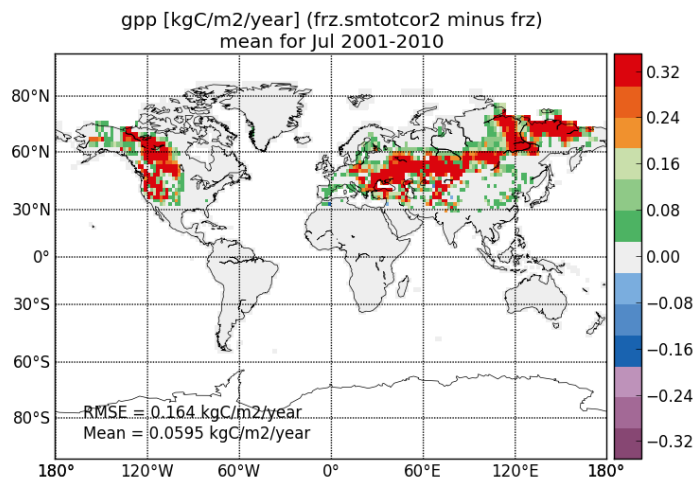
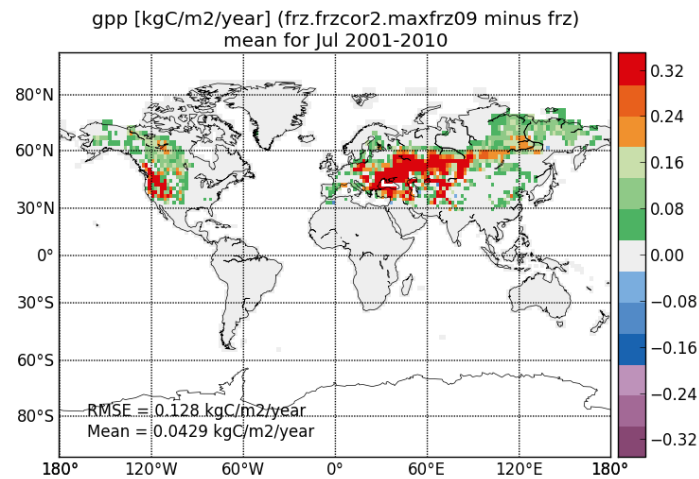
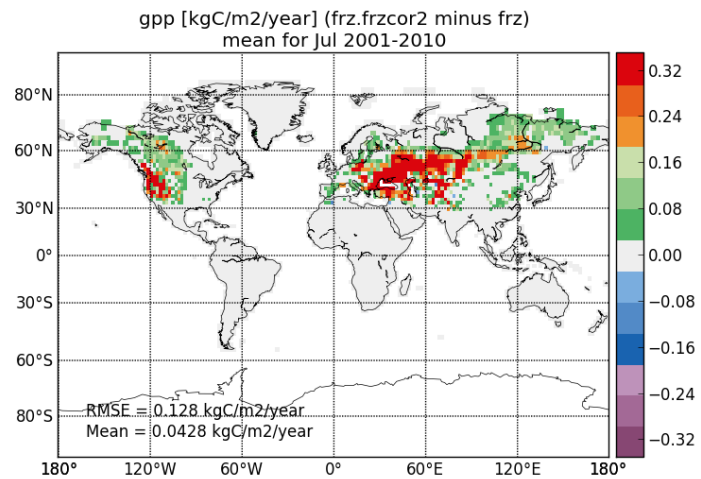


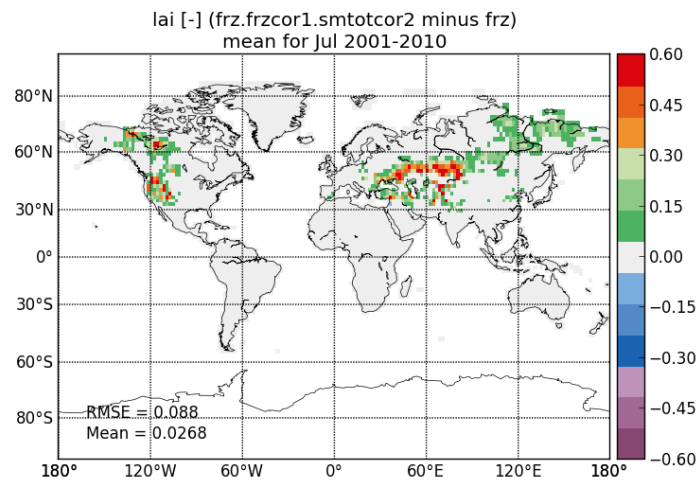
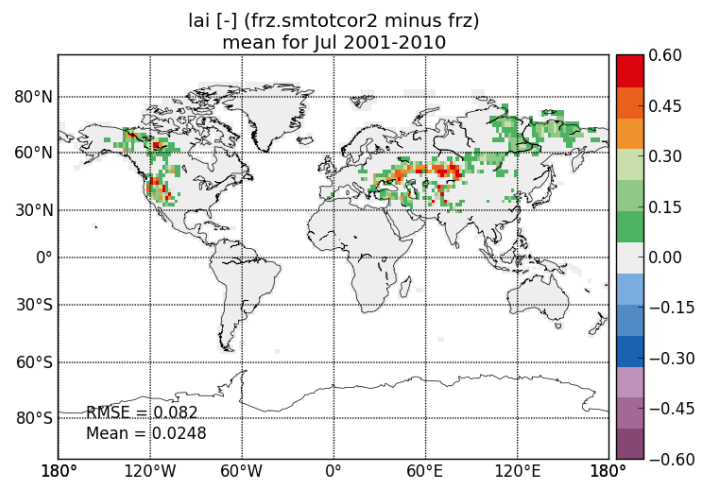
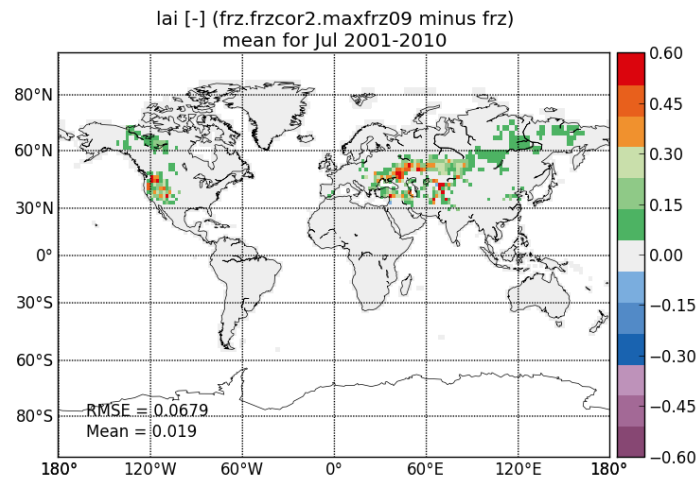
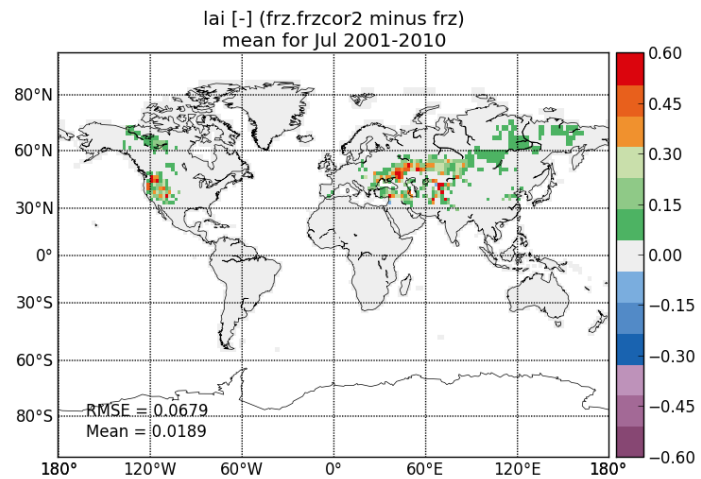
13: Niger (1991-1994)  
(Malanville)



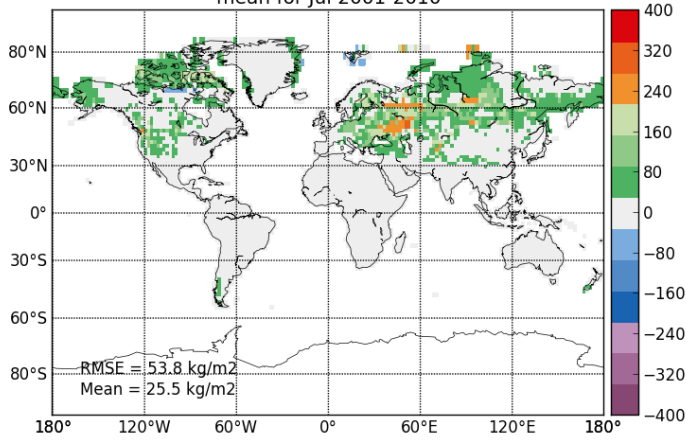
River discharge (m3/s)



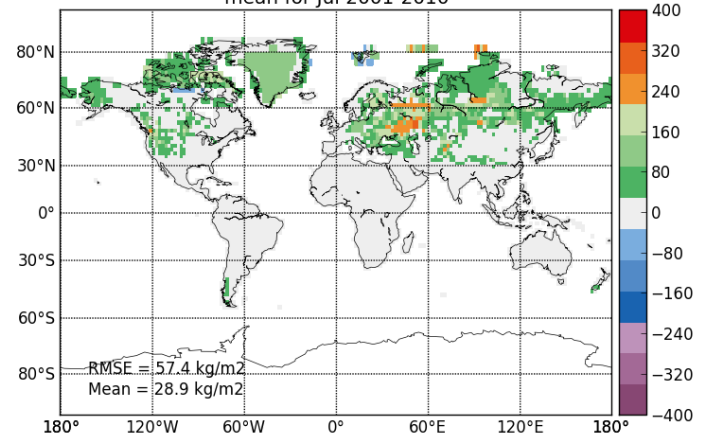




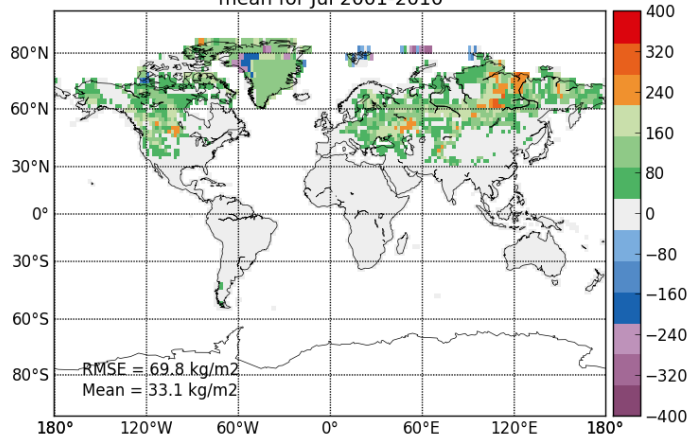
mrso [kg/m<sup>2</sup>] (frz.frzcor2 minus frz)  
mean for Jul 2001-2010



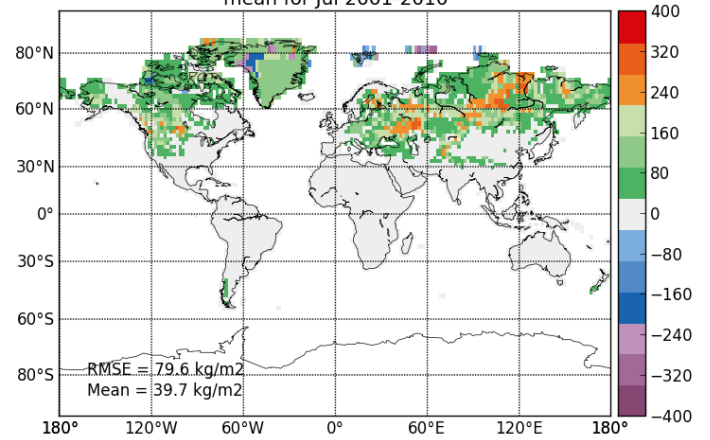
mrso [kg/m<sup>2</sup>] (frz.frzcor2.maxfrz09 minus frz)  
mean for Jul 2001-2010



mrso [kg/m<sup>2</sup>] (frz.smtotcor2 minus frz)  
mean for Jul 2001-2010

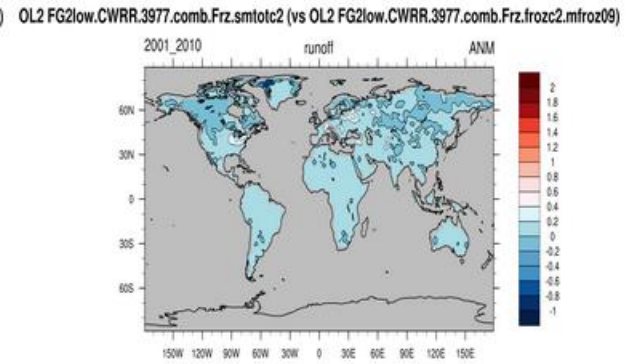
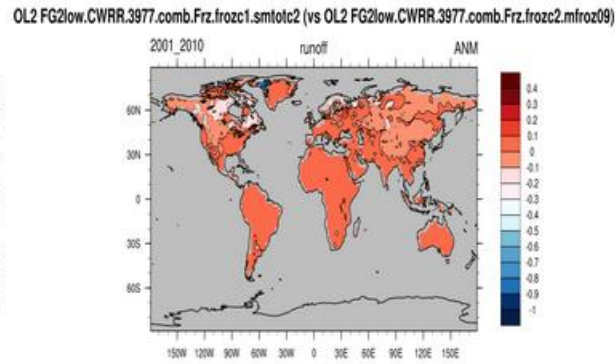
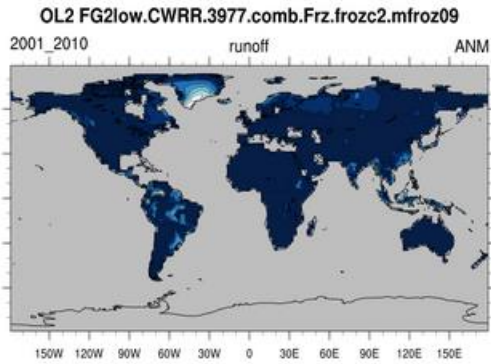


mrso [kg/m<sup>2</sup>] (frz.frzcor1.smtotcor2 minus frz)  
mean for Jul 2001-2010

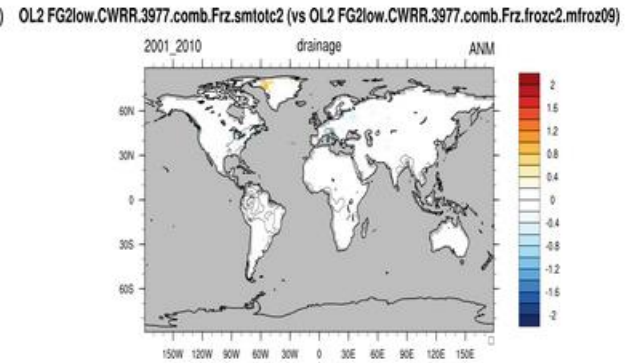
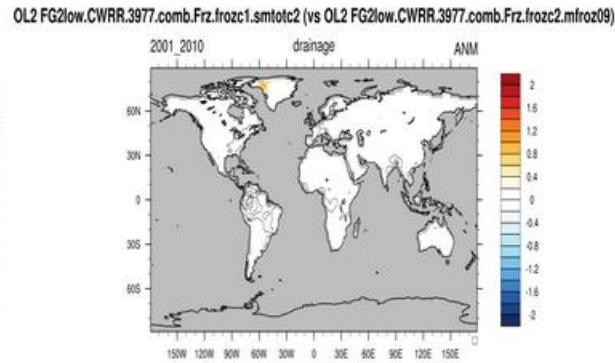
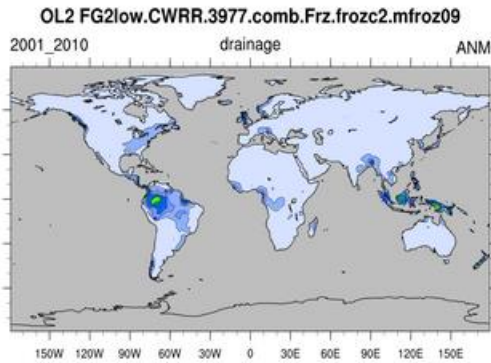




• **Runoff (runoff)**



• **Drainage (drainage)**



# Maps of mean lai (m<sup>-2</sup> m<sup>-2</sup>)

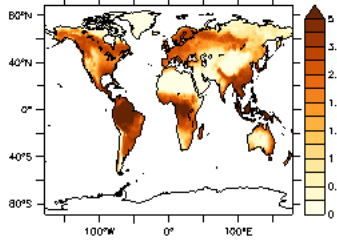
k=@SUM



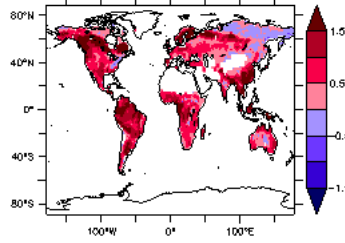
## REF

FG2low\_CWRR\_3977\_comb\_19010101\_20101231\_1M\_lai.nc  
1/CONTRAC[d=1]\*lai x un\_var1

Diff with OBS



Unweighted Avg: 1.753 Std: 1.588 Min: 0 Max: 6.79

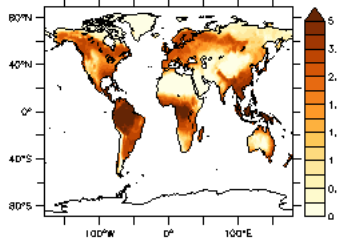


Unweighted Avg: 0.65 Std: 0.679 Min: -1.188 Max: 3.449

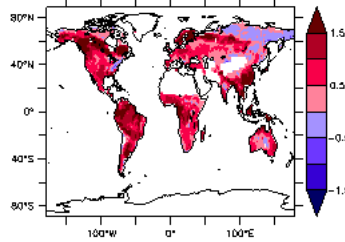
## EVAL

FG2low\_CWRR\_3977\_comb.Frz.frzcor1.smtotc2\_19910101\_20101231\_1M\_lai.nc  
1/CONTRAC[d=2]\*lai x un\_var2

Diff with OBS



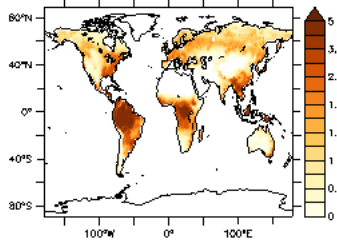
Unweighted Avg: 1.752 Std: 1.587 Min: 0 Max: 6.79



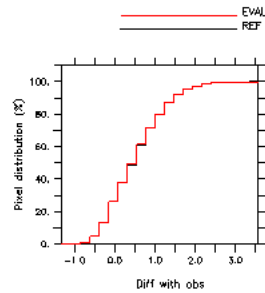
Unweighted Avg: 0.648 Std: 0.678 Min: -1.201 Max: 3.45

## OBS

gimms-LAI-1982\_2009.nc  
0.1\*lai



Unweighted Avg: 1.371 Std: 1.103 Min: 0.071 Max: 5.356



# Maps of mean lai (m<sup>-2</sup> m<sup>-2</sup>)

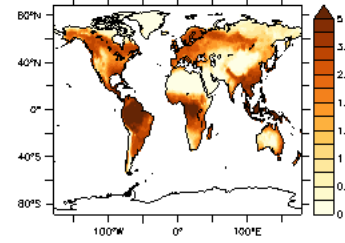
k=@SUM



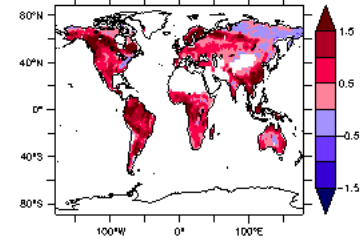
## REF

FG2low\_CWRR\_3977\_comb\_19010101\_20101231\_1M\_lai.nc  
1/CONTRAC[d=1]\*lai x un\_var1

Diff with OBS



Unweighted Avg: 1.753 Std: 1.588 Min: 0 Max: 6.79

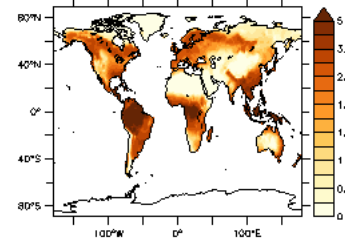


Unweighted Avg: 0.65 Std: 0.679 Min: -1.188 Max: 3.449

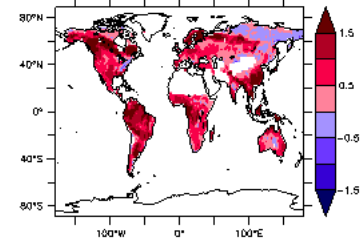
## EVAL

FG2low\_CWRR\_3977\_comb.Frz.smtotc2\_19910101\_20101231\_1M\_lai.nc  
1/CONTRAC[d=2]\*lai x un\_var2

Diff with OBS



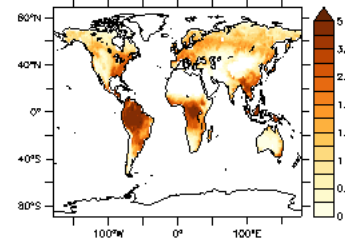
Unweighted Avg: 1.75 Std: 1.587 Min: 0 Max: 6.79



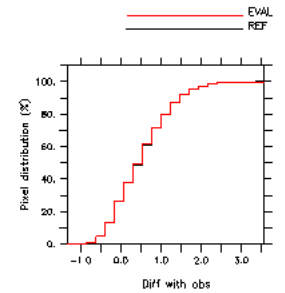
Unweighted Avg: 0.646 Std: 0.679 Min: -1.201 Max: 3.45

## OBS

gimms-LAI-1982\_2009.nc  
0.1\*lai



Unweighted Avg: 1.371 Std: 1.103 Min: 0.071 Max: 5.356



"frz.frzcor1.smtotcor2"

"frz.smtotcor2"

## Bilan :

+ favorable à garder une correction qui prend en compte humidité et température en donnant plus de poids à l'humidité

A tester après modification du calcul du stress hydrique (en ne prenant en compte que la fraction d'eau mobilisable par la plante)

A tester avec d'autres forçages

Mais LAI toujours sous-estimés ...

Problème du LAI<sub>max</sub> pour les PFT 9 et 10 (3 et 2.5 respectivement) ?

Calcul des stress hydriques (cf tests Dan Zhu ) ?