# An example of a RK3 method used in WRF (Wicker and Skamarock, 2002)

$$\phi^* = \phi + \frac{\Delta t}{3} f(\phi)$$

$$\phi^{**} = \phi + \frac{\Delta t}{2} f(\phi^*)$$

$$\phi^+ = \phi + \Delta t f(\phi^{**})$$

- two level time stepping (from n to n+1)
- second evaluation centered (i.e. given at n+1/2)
- 3 evaluations of the RHS
- only the last RHS evaluation contains the vertical mixing.

```
Stage 1 starting:
           U^* = Un ; e3^* = e3n ; tra^* = tra n
         rhs of e3 and dynamics:
           call compute_rhs_dyn( U*, tra*,e3*, rhs_uv, stage=1)
           call compute rhs e3 (U*, e3*
                                            rhs e3
         time advance of e3 and dynamics
           call advance var( e3n, e3*, rhs_e3, e3(stage=1))
           call advance var( Un, e3(n stage), rhs uv, U (stage=1)
         rhs & time advance of tracers
           call compute_rhs_tra(U* , tra*, rhs_tra, n_stage=1)
           call advance var (tra(n), e3, rhs tra, tra(n stage))
        starting: (including diagnostic of w*)
Stage 2
           e3^* = combine dyn e3(e3(n,1),
                                                      , n_stage=2)
           U^* = combine_dyn_u (e3(n,1), u(n,1), e3^*, n_stage=2)
           tra^* = combine dyn tra(tra(n,1))
                                                      , n_stage=2)
         rhs of e3 and dynamics
           call compute_rhs_dyn(U*, tra*, e3*, rhs_uv, n_stage=2)
                                       , e3* , rhs e3
           call compute rhs e3 (U*
         time advance of e3 and dynamics
           call advance_e3 (e3n, e3*,
                                              ,rhs_e3, e3(stage=2) )
           call advance_dyn(un , e3(n_stage),rhs_uv, U (stage=2))
         rhs and time advance of tracers
           call compute rhs tra( U* , tra*, rhs tra, n stage=2)
           call advance_tra (tra_n, e3(n,2), rhs_tra, tra(n_stage))
         starting: centered in n+1/2 and including the diagnostic of \mathbf{w}^*)
Stage 3
           e3* = combine_dyn_e3(e3(n,2))
                                                      , n_stage=3 )
           U^* = combine_dyn_u (e3(n,2), u(0,2), e3^*, n_stage=3)
           tra^* = combine dyn tra(tra(n,2))
                                                      , n stage=3)
         rhs dynamics and its vertical average
           call compute_rhs_dyn( U*, tra*, e3* , rhs_uv, n_stage=3 )
           rhs u ave = average( rhs uv )
         Integrate ssh & e3
           call advance ssh( rhs_uav, ssh(n+1), u2d(n+1/2), u2d(n+1))
           call compute e3( ssh(n+1) , e3(n_stage=3)
         time advance of dynamics (including mixing tendency)
           call advance_dyn( U(1), e3(n_stage=3), rhs_uv, U(n_stage=3))
           call correct_vertical_avergage( u2d(n+1) , U(n_stage=3) )
         rhs and time advance of tracers (including mixing tendency)
           call correct_vertical_avergage( u2d(n+1/2), U* )
           call compute rhs tra( U*, tra*, rhs tra, n stage=3)
           call advance var (tra n, e3, rhs tra, tra(n stage=3))
```

### Various Remarks and questions:

- Forward-Backward Scheme (FBS)
  - ==>> straightforward simplification of above algorithm requires the viscosity to be large (low resolution ocean)
- Requires, for all TRA and DYN tendency routines:
   ==>> pass velocity and/or T-S together with e3 in argument
- How to deal with adaptive, courant-dependent implicit vert. adv.
   ==>> implicit inversion at each stage ???
- How to deal with implicit top and bottom friction
   ==>> adaptation of Jérome's idea to variable e3 ?
- AGRIF compatibility
   ==>> swap from n to n+1 all done at the very end, sufficient ?
- z-tilda coordinate
   ==>> applied at all step (w\* calculation) or only the last one?
- Do we all agree to remove Vector Form (VF)

==>> only available in Flux Form (FF)

pro - significant reduction of the code

- e3t, u, v no more surface weighted quantities, simple average
- A Compensated Time-Space scheme (CTS) will need FF.
- monotonic momentum advection will also need need FF.
- con only energy conserving scheme
  - better shape of baroclinic instability in a channel....

- ...

- Coriolis: FF, f-parameter defined at T-point. but issue with its vertical average with step or partial step topography (issue that exist also with Coriolis defined at F-point.
- Passive tracers: not inside the RK3 framework possible ?
   ==>>> single time integration (with possibly time coarsening)
- Pressure gradient : for sco, mix sco-zps and z-tilda coordinate. :
   ==>> pressure gradient using finit volume form ?

#### **Proposed implementation strategy:**

#### Initial target:

RK3 with WRF choice (known to work, but probably not optimal) as separate directory

## preparation phase : (shared with the dev\_merge\_2017 (DM2017) )

- Coriolis at T-point (Done and ready for DM2017)
- pass in argument U,T, e3 in all DYN/TRA (Done, and verified one by one in LF case. Put this in DM2017?)
- time-integration of (e3t T) (shared with DM2017)
- dynspg\_ts: split of 2Δt/Δt calculation (shared with DM2017?)

### **RK3 directory only:**

- suppress the Vector Form (share with DM2017 or not ?)
- implement and test
- Surface Module: forcing provided at n+1/2 only. adjust the sea-ice and iceberg time-step.

### Work in parallel:

- Adaptive Courant-number-dependent implicit vertical advection:
   1st in MLF case, then try to find an optimize solution for RK3 needed to obtain the largest possible time-step.
- // dynspg\_ts : move to a RK3 framework (cf Laurent/Rachid work)
- // dynspg\_ts : add momentum non-linear terms ?
- // hpg : finite volume pressure gradient consistent with TEOS10
- Coriolis: test the effect of a clean removal of barotopic Coriolis trend for the 2D RHS of external mode with step-like topography.
- // determine the optimal RK3 choice.

# Second stage:

- incorporate the work done in //
- · adaptation to passive tracer
- AGRIF compatibility
- and a lot of tests...